

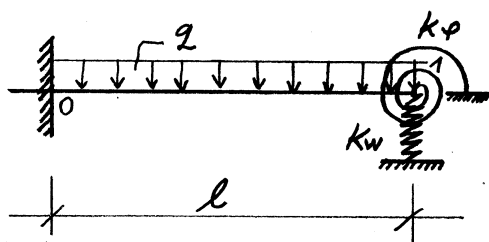
1. Rešitev mehanskega problema trdnega telesa je matrika majhnih deformacij ϵ_{ij} . V točki $T(2, 2, 0)$ določi:

- velikosti glavnih normalnih napetosti
- deformirano materialno koordinatno bazo

$$[\epsilon_{ij}] = 10^{-3} \cdot \begin{array}{|c|c|c|} \hline 10x & y^2 & 0 \\ \hline y^2 & 4xy & 0 \\ \hline 0 & 0 & 0 \\ \hline \end{array}$$

$$\begin{aligned} 2\mu &= 16000 \text{ kN/cm}^2 \\ \lambda &= 8000 \text{ kN/cm}^2 \end{aligned}$$

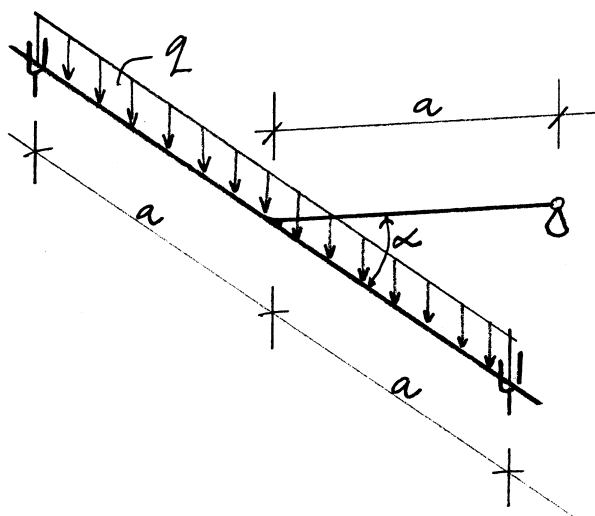
2. Nosilec je v točki 1 elastično podprt. Konstanta linearne vzmeti je k_w , konstanta spiralne vzmeti pa je k_p . Določi pomike in zasuke obeh podpor!



$$\begin{aligned} l &= 4 \text{ m} \\ q &= 0,1 \text{ MN/m} \\ EI_y &= 4 \text{ MNm}^2 \\ k_w &= 1 \text{ MN/m} \\ k_p &= 0,05 \text{ MNm/rad} \end{aligned}$$

*

3. Določi in skiciraj notranje sile!



$$\begin{aligned} \alpha &= 60^\circ \\ EI_y &= G I_x \end{aligned}$$

Ad 1.

$$a) \quad [\varepsilon_{ij}]_T = 10^{-3} \begin{bmatrix} 20 & 4 & 0 \\ 4 & 16 & 0 \\ 0 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 0,020 & 0,004 & 0 \\ 0,004 & 0,016 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\varepsilon_{11,22} = 10^{-3} \left(\frac{20+16}{2} \pm \sqrt{\left(\frac{20-16}{2}\right)^2 + 4^2} \right)$$

$$\varepsilon_{11} = 22,47 \cdot 10^{-3}$$

$$\varepsilon_{22} = 13,53 \cdot 10^{-3}$$

$$\sigma_{11} = 2\mu \varepsilon_{11} + \lambda (\varepsilon_{11} + \varepsilon_{22}) \rightarrow$$

$$\sigma_{11} = 648 \text{ kN/cm}^2$$

$$\sigma_{22} = 2\mu \varepsilon_{22} + \lambda (\varepsilon_{11} + \varepsilon_{22}) \rightarrow$$

$$\sigma_{22} = 504 \text{ kN/cm}^2$$

$$\sigma_{33} = \lambda (\varepsilon_{11} + \varepsilon_{22}) \rightarrow$$

$$\sigma_{33} = 288 \text{ kN/cm}^2$$

b) Za referenčno točko izberemo $T_0(0,0,0)$:

$$\omega_z = \omega_z(T_0) + \int_0^x \vec{e}_z (\vec{\nabla} \times \vec{E}_x)_{y=0} dx + \int_0^y \vec{e}_z (\vec{\nabla} \times \vec{E}_y) dy$$

$$\vec{e}_z (\vec{\nabla} \times \vec{E}_x) = \begin{vmatrix} 0 & 0 & 1 \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_{xx} & E_{xy} & 0 \end{vmatrix} = \varepsilon_{yx,x} - \varepsilon_{xx,y} = 0$$

$$\vec{e}_z (\vec{\nabla} \times \vec{E}_y) = \begin{vmatrix} 0 & 0 & 1 \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_{yx} & E_{yy} & 0 \end{vmatrix} = \varepsilon_{yy,x} - \varepsilon_{xy,y} = 2y \cdot 10^{-3}$$

$$\omega_z = \omega_z(T_0) + 10^{-3} \cdot \int_0^y 2y dy = \underline{\underline{\omega_z(T_0) + 10^{-3} \cdot y^2}}$$

$$u_x = u_x(T_0) + \int_0^x \epsilon_{xx}|_{y=0} dx + \int_0^y (\epsilon_{yx} - \omega_z) dy$$

$$u_x = u_x(T_0) + 10^{-3} \left[\int_0^x 10x dx + \int_0^y (y^2 - \omega_z^0 \cdot 10^3 - y^2) dy \right]$$

$$u_x = u_x(T_0) + 5x^2 \cdot 10^{-3} - \omega_z^0 \cdot y$$

$$u_y = u_y(T_0) + \int_0^x (\epsilon_{xy} + \omega_z)|_{y=0} dx + \int_0^y \epsilon_{yy} dy$$

$$u_y = u_y(T_0) + 10^{-3} \left[\int_0^x (y^2 + \omega_z^0 \cdot 10^3 + y^2) dx + \int_0^y 4xy dy \right]$$

$$u_y = u_y(T_0) + \omega_z^0 \cdot x + 2xy^2 \cdot 10^{-3}$$

$$\vec{e}_x' = \vec{e}_x + \frac{\partial \vec{u}}{\partial x} = \vec{e}_x + 10x \cdot 10^{-3} \vec{e}_x + (\omega_z^0 + 2y^2 \cdot 10^{-3}) \vec{e}_y$$

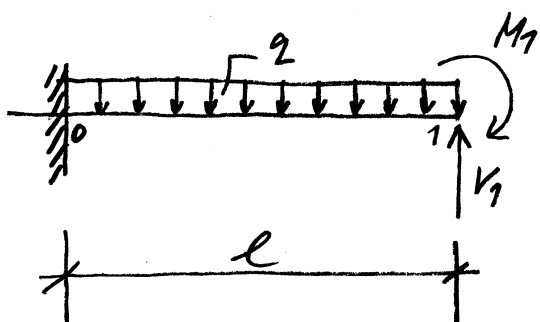
$$\vec{e}_y' = \vec{e}_y + \frac{\partial \vec{u}}{\partial y} = \vec{e}_y - \omega_z^0 \vec{e}_x + 4xy \cdot 10^{-3} \vec{e}_y$$

V točki $T(2, 2, 0)$:

$$\vec{e}_x' = 1,020 \vec{e}_x + (\omega_z^0 + 0,080) \vec{e}_y$$

$$\vec{e}_y' = -\omega_z^0 \vec{e}_x + 1,016 \vec{e}_y$$

Ad 2.



$$M_1 = k_p \cdot \omega_1$$

$$V_1 = k_w \cdot \omega_1$$

$$w_1 = \frac{2l^4}{8EI_y} - k_w w_1 \frac{l^3}{3EI_y} + k_p w_1 \frac{l^2}{2EI_y}$$

$$w_1 = -\frac{2l^3}{6EI_y} + k_w w_1 \frac{l^2}{2EI_y} - k_p w_1 \frac{l}{EI_y}$$

$$w_1 \left(1 + \frac{k_w l^3}{3EI_y}\right) - w_1 \frac{k_p l^2}{2EI_y} = \frac{2l^4}{8EI_y}$$

$$w_1 \frac{k_w l^2}{2EI_y} - w_1 \left(1 + \frac{k_p l}{EI_y}\right) = \frac{2l^3}{6EI_y}$$

6,333	-0,1
2	-1,05

w_1	=	0,8
w_1	=	0,2667

$$\text{Det} = -6,45$$

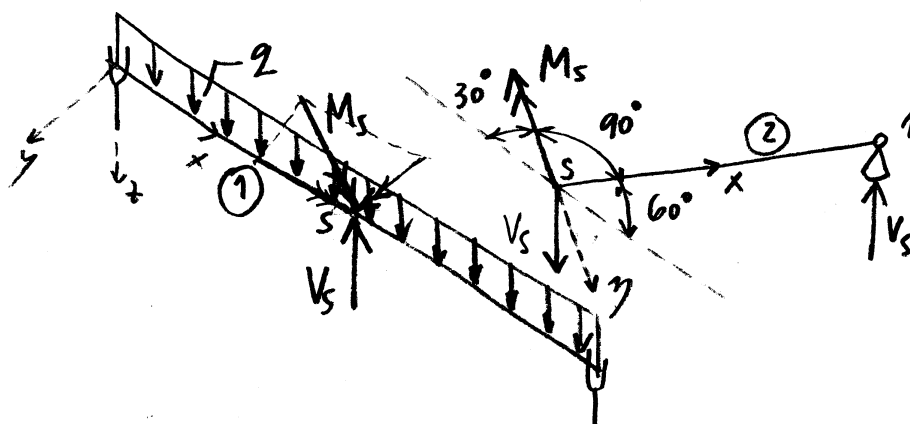
$$\delta_1 = -0,8133 \rightarrow$$

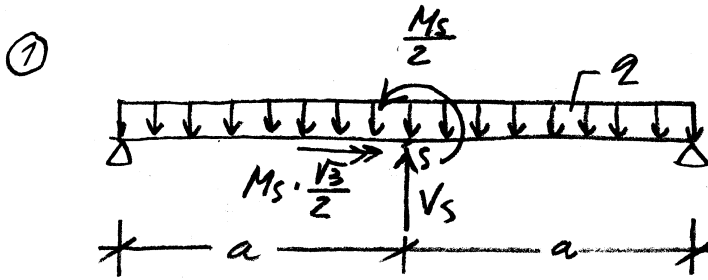
$$\delta_2 = -0,0889 \rightarrow$$

$$w_1 = 0,126 \text{ m}$$

$$w_1 = 0,0138 \text{ rad}$$

AM 3.





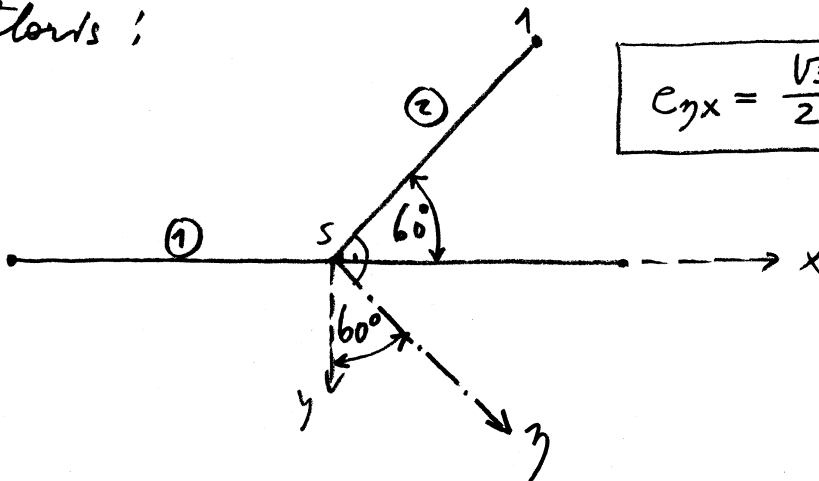
$$w_s = \frac{5q(2a)^4}{384EI_y} - \frac{V_s(2a)^3}{48EI_y}$$

$$w_s = \frac{5qa^4}{24EI_y} - \frac{V_s a^3}{6EI_y}$$

$$w_y^s = \frac{Ms a}{12EI_y}$$

$$w_x^s = \frac{Ms\sqrt{3} a}{4GI_x}$$

Floris :

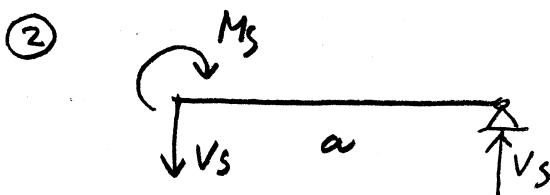


$$e_{\eta x} = \frac{\sqrt{3}}{2} \quad e_{\eta y} = \frac{1}{2}$$

$$w_{\eta}^{(2)}(s) = w_x^s e_{\eta x} + w_y^s e_{\eta y} = \frac{Ms\sqrt{3} a}{4GI_x} \cdot \frac{\sqrt{3}}{2} + \frac{Ms a}{12EI_y} \cdot \frac{1}{2}$$

$$w_{\eta}^{(2)}(s) = \frac{Ms a}{EI_y} \left(\frac{3}{8} + \frac{1}{24} \right) \rightarrow w_{\eta}^{(2)}(s) = \frac{5Ms a}{12EI_y}$$

$$w_1 = w_s - a w_{\eta}^{(2)}(s) - V_s \cdot \frac{a^3}{3EI_y} = 0 !$$



$$V_s = \frac{Ms}{a}$$

$$W_1 = \frac{52a^4}{24EI_y} - \frac{M_s a^2}{6EI_y} - \frac{5M_s a^2}{12EI_y} - \frac{M_s a^2}{3EI_y} = 0$$

$$M_s \left(\frac{1}{6} + \frac{5}{12} + \frac{1}{3} \right) = \frac{52a^2}{24} \rightarrow$$

$M_s = \frac{52a^2}{22}$
$V_s = \frac{52a}{22}$