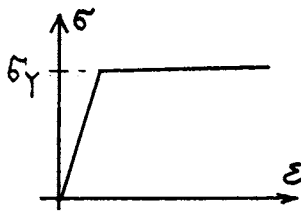


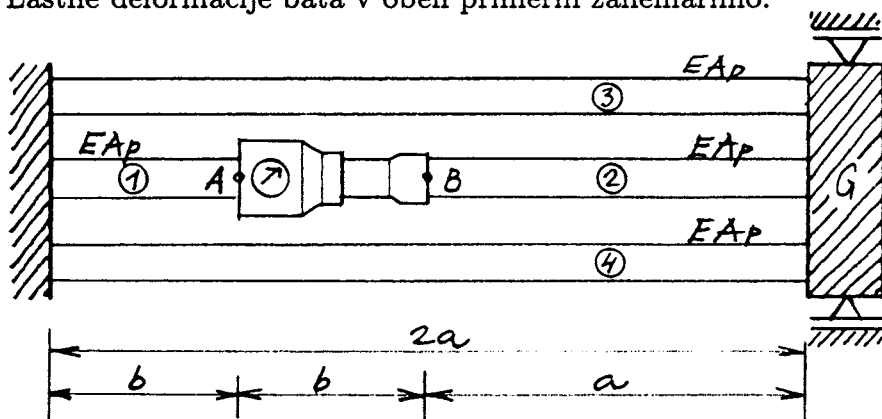
1. Napetostno stanje delca \mathcal{D} je opisano s komponentami σ_{ij} tenzorja napetosti glede na koordinatni sistem (x, y, z) .
- Dokaži, da je ravnina, π_ζ , katere normala e_ζ oklepa enake kote z osmi x, y, z , ena od glavnih ravnin podanega napetostnega stanja! Določi preostali dve glavni ravnini in vse glavne normalne napetosti!
 - Določi specifično spremembo prostornine, ki pripada obravnavanemu delcu \mathcal{D} (modul elastičnosti E in koeficient prečne kontrakcije ν sta podani vrednosti)!
 - Obravnavano telo je narejeno iz bilinearnega elastično-plastičnega materiala. Pri enoosnem napetostnem stanju je prehod iz elastičnega v plastično stanje določen z mejo plastičnega tečenja σ_Y . Upoštevajoč Misesov pogoj tečenja določi napetost q_Y , pri kateri pri podanem prostorskem napetostnem stanju delca \mathcal{D} nastopijo prve plastične deformacije! Napetost q_Y izrazi v odvisnosti od σ_Y !



$$[\sigma_{ij}] = \begin{bmatrix} q & 2q & 2q \\ 2q & q & 2q \\ 2q & 2q & q \end{bmatrix}$$

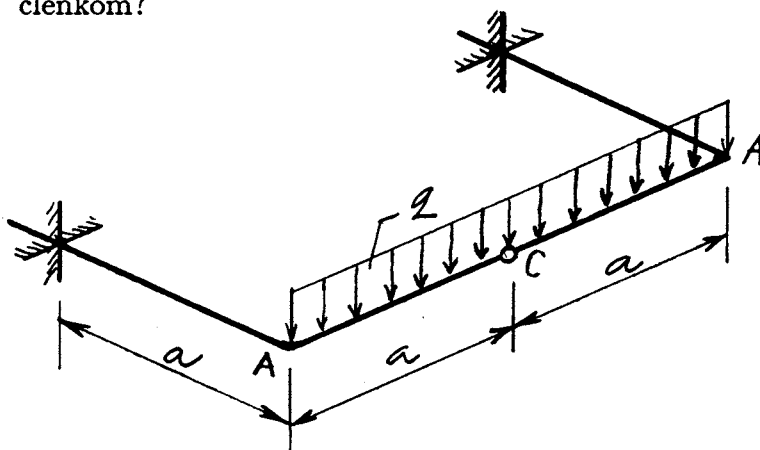
2. Med palici 1 in 2 vstavimo bat hidravlične naprave. V začetku med batom in palicama ni napetosti.
- Določi potrebno silo v batu, pri kateri se razdalja med točkama A in B poveča za $\delta = 2 \text{ mm}$! Kolikšne so tedaj napetosti v palicah?
 - Določi potrebno silo v batu, pri kateri se razdalja med točkama A in B ne spremeni, če palici 1 in 2 segrejemo za $\Delta T = 60 \text{ K}$, palici 3 in 4 pa obdržita začetno temperaturo! Določi premik toge vezne grede G!

Lastne deformacije bata v obeh primerih zanemarimo.



$$\begin{aligned} E &= 200\,000 \text{ MPa} \\ \alpha_T &= 1.25 \cdot 10^{-5} / \text{K} \\ a &= 2 \text{ m} \\ b &= 1 \text{ m} \\ A_p &= 10 \text{ cm}^2 \end{aligned}$$

3. Določi navpični pomik točke C! Kako se spremeni ta pomik, če nosilec v točki C ni prekinjen s členkom?



$$\begin{aligned} q &= 0.1 \text{ MN/m} \\ EI_y &= GI_x = 100 \text{ MNm}^2 \\ a &= 3 \text{ m} \end{aligned}$$

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Ad 1.

$$a) \sigma_{fx} = \sigma_{fy} = \sigma_{fz} \rightarrow 3\sigma_{fx}^2 = 1 \rightarrow \sigma_{fx} = \frac{1}{\sqrt{3}}$$

$$\vec{e}_f = \frac{1}{\sqrt{3}} (\vec{e}_x + \vec{e}_y + \vec{e}_z)$$

$$\begin{Bmatrix} \sigma_{fx} \\ \sigma_{fy} \\ \sigma_{fz} \end{Bmatrix} = \begin{bmatrix} 2 & 2q & 2q \\ 2q & 2 & 2q \\ 2q & 2q & 2 \end{bmatrix} \cdot \frac{1}{\sqrt{3}} \begin{Bmatrix} 1 \\ 1 \\ 1 \end{Bmatrix} = \frac{5}{\sqrt{3}} \begin{Bmatrix} 2 \\ 2 \\ 2 \end{Bmatrix}$$

$$\vec{\sigma}_f = \frac{5q}{\sqrt{3}} (\vec{e}_x + \vec{e}_y + \vec{e}_z)$$

$$\sigma_{ff} = \vec{\sigma}_f \cdot \vec{e}_f = \frac{5q}{3} (1+1+1) \rightarrow \boxed{\sigma_{ff} = 5q}$$

$$\vec{\sigma}_f = \sigma_{ff} \vec{e}_f$$

$$b) \boxed{\sigma_{ff} = \sigma_{33} = 5q}$$

$$I_1 = 3q$$

$$I_2 = 3 \begin{vmatrix} q & 2q \\ 2q & q \end{vmatrix} = -9q^2$$

$$I_3 = q(q^2 - 4q^2) - 2q(2q^2 - 4q^2) + 2q(4q^2 - 2q^2)$$

$$I_3 = 5q^3$$

$$\boxed{\sigma^3 - I_1 \sigma^2 + I_2 \sigma - I_3 = 0} \rightarrow$$

$$\sigma^3 - 3q\sigma^2 - 9q^2\sigma - 5q^3 = 0$$

$$\begin{array}{r} (\sigma^3 - 3q\sigma^2 - 9q^2\sigma - 5q^3) : (\sigma - 5q) = \sigma^2 + 2q\sigma + q^2 \\ -\sigma^3 + 5q\sigma^2 \\ \hline 2q\sigma^2 - 9q^2\sigma \\ -2q\sigma^2 + 10q^2\sigma \\ \hline q\sigma - 5q^3 \\ \hline q\sigma - 5q^3 \\ \hline 0 \end{array}$$

$$\sigma^2 + 2\sigma + 2^2 = 0 \rightarrow \boxed{\sigma_{11} = \sigma_{22} = -2}$$

2

Glavna smer $\vec{e}_3 \equiv \vec{e}_\xi$, glavni smeri \vec{e}_1 in \vec{e}_2 sta pravokotni na \vec{e}_ξ , oster pa poljubni, ker je $\sigma_{11} = \sigma_{22}$!

$$b) \boxed{I_1^\sigma = 3\sigma}$$

$$I_1^\epsilon \approx \epsilon_V = \frac{1-2\nu}{E} I_1^\sigma$$

$$\boxed{\epsilon_V = \frac{3(1-2\nu)}{E} \sigma}$$

$$a) \text{ Mises: } (\sigma_{11} - \sigma_{22})^2 + (\sigma_{22} - \sigma_{33})^2 + (\sigma_{33} - \sigma_{11})^2 = 6 k_M^2$$

$$\sigma_{22} = \sigma_{33} = 0 \rightarrow 2\sigma_{11}^2 = 6 k_M^2 \rightarrow \sigma_{11}^2 = 3 k_M^2$$

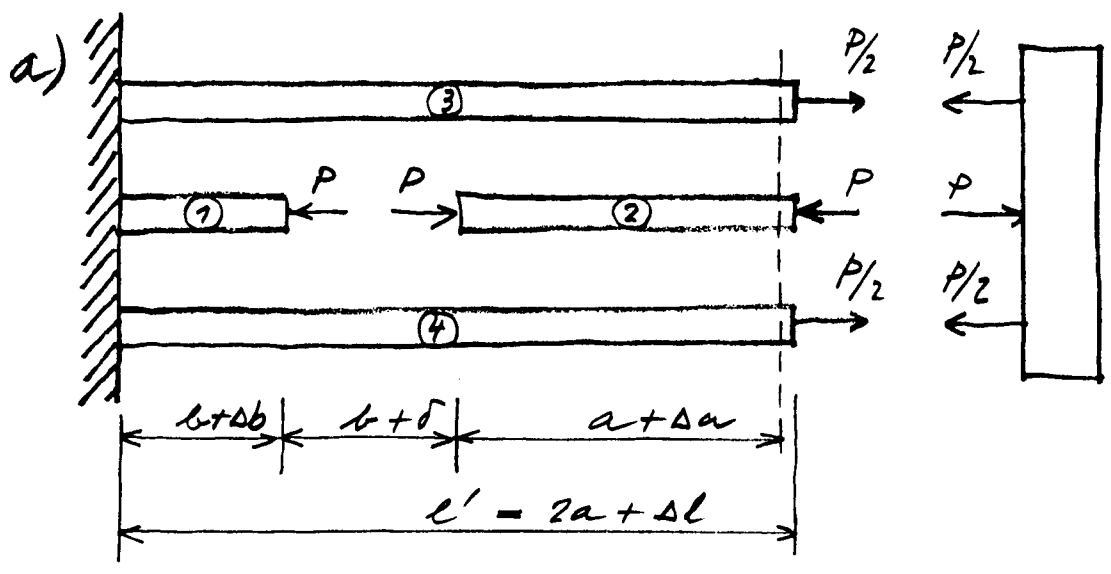
$$\sigma_{11} = \sigma_Y \rightarrow \boxed{k_M = \frac{1}{\sqrt{3}} \sigma_Y}$$

$$\boxed{(\sigma_{11} - \sigma_{22})^2 + (\sigma_{22} - \sigma_{33})^2 + (\sigma_{33} - \sigma_{11})^2 = 2\sigma_Y^2}$$

$$\boxed{\sigma_{11} = \sigma_{22} = -\sigma, \quad \sigma_{33} = 5\sigma :}$$

$$0 + 36\sigma^2 + 36\sigma^2 = 2\sigma_Y^2 \rightarrow \boxed{\sigma_Y = \frac{1}{6} \sigma_Y}$$

Ad 2.)



$$l' = 2a + \frac{P}{2} \cdot \frac{2a}{EA_P} = \left(b - P \frac{b}{EA_P}\right) + \left(a - P \frac{a}{EA_P}\right) + (b + \delta)$$

$$P \frac{1}{EA_P} (a + b + a) = b + a + b + \delta - 2a$$

$$2b + a = 2a \rightarrow \boxed{P = \frac{\delta EA_P}{2a + b}} \rightarrow \boxed{P = 80 \text{ kN}}$$

$$b) \quad l' = 2a + \frac{P}{2} \frac{2a}{EA_P} =$$

$$= \left(b - P \frac{b}{EA_P} + b \alpha_T \Delta T\right) + \left(a - P \frac{a}{EA_P} + a \alpha_T \Delta T\right) + b$$

$$\frac{P}{EA_P} (2a + b) = 2a - 2a + (a + b) \alpha_T \Delta T$$

$$\boxed{P = \frac{a + b}{2a + b} EA_P \alpha_T \Delta T} \rightarrow \boxed{P = 90 \text{ kN}}$$

$$\boxed{u_G = P \frac{a}{EA_P}} \rightarrow \boxed{u_G = 0,09 \text{ cm}}$$

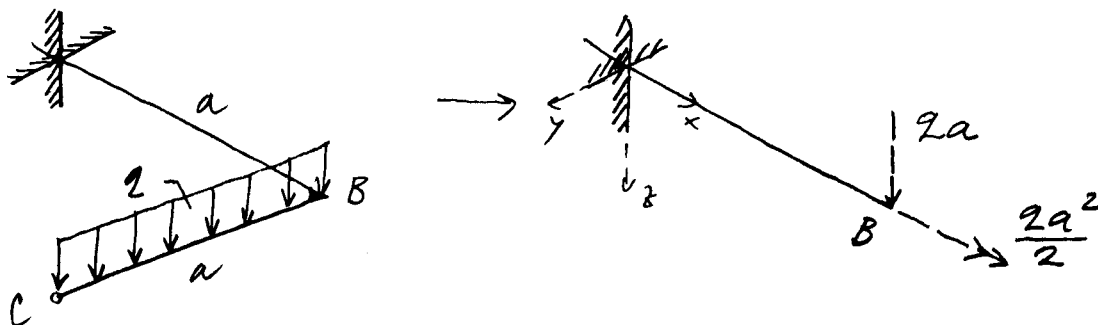
a) Napetosti v posameznih :

$$\textcircled{1}, \textcircled{2} \rightarrow \boxed{\sigma = -8 \text{ kN/cm}^2} \quad \textcircled{3}, \textcircled{4} \rightarrow \boxed{\sigma = 4 \text{ kN/cm}^2}$$

Ad 3.)

a) člen v tržní c:

4



$$\omega_x(B) = \frac{2a^2}{2} \cdot \frac{q}{GI_x} = 2 \frac{a^3}{2GI_x}$$

$$\omega_B = 2a \frac{a^3}{3EI_y} = 2 \frac{a^4}{3EI_y}$$

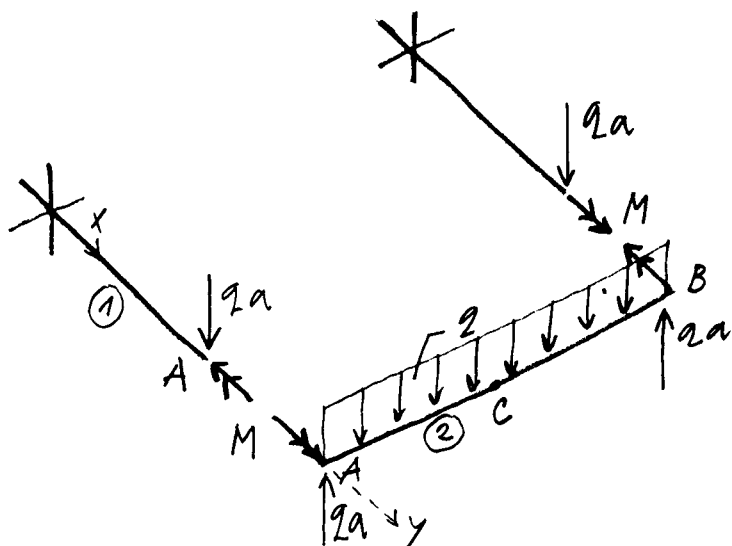
$$\omega_C = \omega_B + \omega_x(B) \cdot a + \frac{2a^4}{8EI_y}$$

$$EI_y = GI_x \rightarrow \omega_C = \frac{2a^4}{EI_y} \left(\frac{1}{3} + \frac{1}{2} + \frac{1}{8} \right)$$

$$\omega_C = 2 \frac{23a^4}{24EI_y}$$

$$\omega_C = 0,0776 \text{ m}$$

b) bez členka:



$$\textcircled{1}: \omega_A^{\textcircled{1}} = 2 \frac{a^4}{3EI_y}$$

$$\omega_x^{\textcircled{1}}(A) = \omega_y^{\textcircled{2}}(A) = -M \frac{a}{GI_x}$$

\textcircled{2}:

$$\omega_y^{\textcircled{2}}(A) = -2 \frac{(2a)^3}{24EI_y} + M \frac{2a}{2EI_y}$$

$$\omega_y^{\textcircled{2}}(A) = -2 \frac{a^3}{3EI_y} + M \frac{a}{EI_y}$$

$$\omega_x^{\textcircled{1}}(A) = \omega_y^{\textcircled{2}}(A) \dots -M \frac{a}{GI_x} = -2 \frac{a^3}{3EI_y} + M \frac{a}{EI_y}$$

$$EI_y = GI_x \dots \quad M = 2 \frac{a^2}{6}$$

$$w_c = w_A + 2 \frac{5(2a)^4}{384 E I_y} - M \frac{(2a)^2}{8 E I_y}$$

$$w_c = 2 \frac{11a^4}{24 E I_y}$$

→

$$w_c = 0,0371 \text{ m}$$