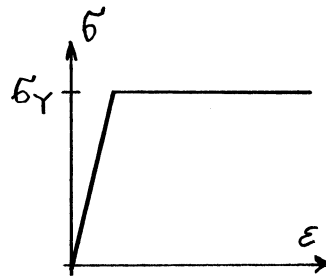
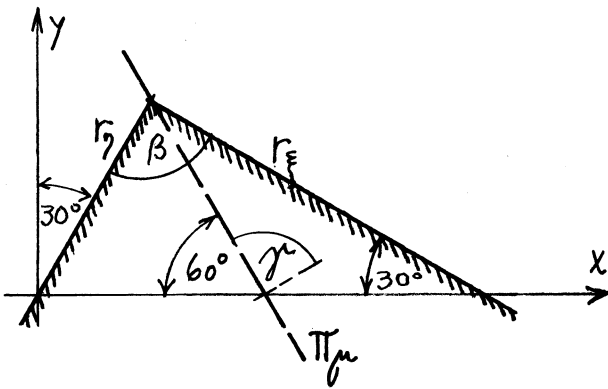


1. Na vogalu enakomerno debele homogene stene, v kateri vlada **homogeno ravninsko napetostno stanje**, izrežemo elementarni del, kakor je prikazano na skici. Na robu r_ξ deluje enakomerna zvezna obtežba $\vec{p}_\xi = -q(\vec{e}_x + \sqrt{3}\vec{e}_y)$, na robu r_η pa enakomerna zvezna obtežba $\vec{p}_\eta = 3q(-\sqrt{3}\vec{e}_x + \vec{e}_y)$.
- Skiciraj obtežbo ter ustrezni zunanji normalni robovi obravnavane stene!
 - Določi komponente tenzorja napetosti glede na kartezijski koordinatni sistem (x, y, z) !
 - Določi rezultirajoči vektor napetosti v ravnini Π_μ z njegovimi komponentami v koordinatnem sistemu (x, y, z) ter normalno in strižno napetost v tej ravnini!
 - Določi spremembi pravih kotov β in γ v odvisnosti od obtežbe q !
 - Določi velikosti in smeri glavnih normalnih napetosti!
 - Obravnavano telo je narejeno iz bilinearne elastično-plastičnega materiala. Pri enoosnem napetostnem stanju je prehod iz elastičnega v plastično stanje določen z mejo plastičnega tečenja σ_Y . Upoštevajoč Misesov pogoj tečenja določi obtežbo q_Y , pri kateri pri podanem napetostnem stanju nastopijo prve plastične deformacije!



$$E = 200\,000 \text{ MPa}$$

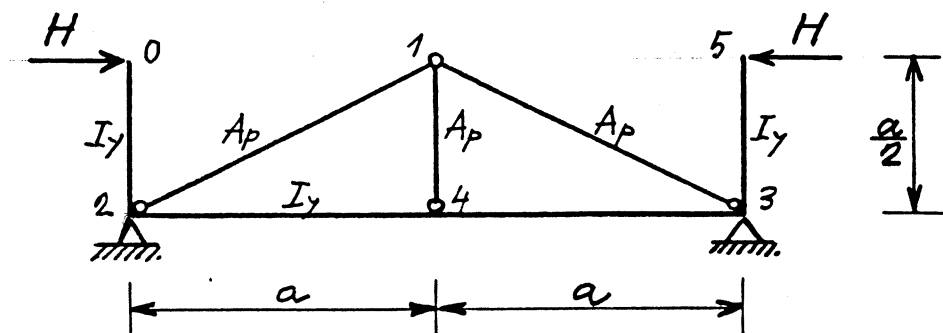
$$\sigma_Y = 360 \text{ MPa}$$

$$\nu = 0.3$$

2. Na jeklen valj premera $D_v = 200 \text{ mm}$ želimo nataktni jekleno cev z notranjim premerom $D_0 = 199.8 \text{ mm}$. Debelina stene cevi je $\delta = 2.2 \text{ mm}$. Trenje med valjem in cevjo je zanemarljivo. V vzdolžni smeri se lahko cev in valj neovirano deformirata.
- Za koliko moramo segreti cev, da bi jo lahko nataktni na valj?
 - Določi napetosti v valju in cevi po ohladitvi sestava na prvotno temperaturo!
 - Določi premer valja po ohladitvi!

$$E = 200\,000 \text{ MPa}, \quad \nu = 0.3, \quad \alpha_T = 1.25 \cdot 10^{-5} / \text{K}.$$

3. Nosilec $\overline{05}$ je podprt s trikotnim vešalom. Določi vodoravni pomik točke 0!



$$H = 0.3 \text{ MN}$$

$$E = 200\,000 \text{ MPa}$$

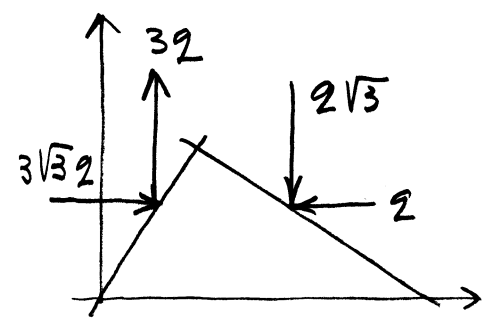
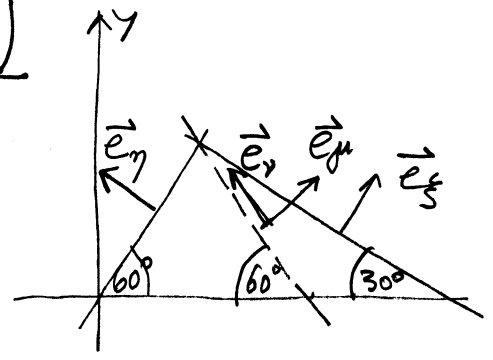
$$A_p = 56 \text{ cm}^2$$

$$I_y = 5400 \text{ cm}^4$$

$$a = 4 \text{ m}$$

Ad 1.)

a)



b) $r_\xi: \vec{e}_\xi = \frac{1}{2}(\vec{e}_x + \sqrt{3}\vec{e}_y) \rightarrow \vec{p}_\xi = -2(\vec{e}_x + \sqrt{3}\vec{e}_y)$

$r_\eta: \vec{e}_\eta = \frac{1}{2}(-\sqrt{3}\vec{e}_x + \vec{e}_y) \rightarrow \vec{p}_\eta = 32(-\sqrt{3}\vec{e}_x + \vec{e}_y)$

$p_{\xi x} = -2 = \frac{1}{2}\sigma_{xx} + \frac{\sqrt{3}}{2}\sigma_{xy} \rightarrow \sigma_{xx} + \sqrt{3}\sigma_{xy} = -2q \quad (A)$

$p_{\xi y} = -2\sqrt{3} = \frac{1}{2}\sigma_{xy} + \frac{\sqrt{3}}{2}\sigma_{yy} \rightarrow \sqrt{3}\sigma_{yy} + \sigma_{xy} = -2\sqrt{3}q \quad (B)$

$p_{\eta x} = -3\sqrt{3}q = -\frac{\sqrt{3}}{2}\sigma_{xx} + \frac{1}{2}\sigma_{xy} \rightarrow \sqrt{3}\sigma_{xx} - \sigma_{xy} = 6\sqrt{3}q \quad (C)$

$p_{\eta y} = 3q = -\frac{\sqrt{3}}{2}\sigma_{xy} + \frac{1}{2}\sigma_{yy} \rightarrow \sigma_{yy} - \sqrt{3}\sigma_{xy} = 6q \quad (D)$

$(B) \rightarrow 3\sigma_{yy} + \sqrt{3}\sigma_{xy} = -6q$
 $(D) \rightarrow \sigma_{yy} - \sqrt{3}\sigma_{xy} = 6q \quad \oplus \rightarrow \boxed{\sigma_{yy} = 0}$

$(B) \rightarrow \boxed{\sigma_{xy} = -2\sqrt{3}q} \quad (A) \rightarrow \boxed{\sigma_{xx} = 4q}$

Kontrola: $(C) \rightarrow 4\sqrt{3}q + 2\sqrt{3}q = 6\sqrt{3}q \quad \checkmark$

$[\sigma_{ij}] = \begin{bmatrix} 4q & -2\sqrt{3}q & 0 \\ -2\sqrt{3}q & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$

c) $\begin{Bmatrix} \sigma_{\mu x} \\ \sigma_{\mu y} \\ \sigma_{\mu z} \end{Bmatrix} = [\sigma_{ij}] \begin{Bmatrix} e_{\mu x} \\ e_{\mu y} \\ e_{\mu z} \end{Bmatrix}$

$\vec{e}_\mu = \frac{1}{2}(\sqrt{3}\vec{e}_x + \vec{e}_y)$

$\vec{e}_\nu = \frac{1}{2}(-\vec{e}_x + \sqrt{3}\vec{e}_y)$

$\boxed{\vec{\sigma}_\mu = 2\sqrt{3}q\vec{e}_x - 3q\vec{e}_y}$

$$\begin{aligned} \sigma_{\mu\mu} &= \vec{\sigma}_{\mu} \vec{e}_{\mu} \rightarrow \sigma_{\mu\mu} = 0 \\ \sigma_{\mu\nu} &= \vec{\sigma}_{\mu} \vec{e}_{\nu} \rightarrow \sigma_{\mu\nu} = -2q\sqrt{3} \end{aligned}$$

$$d) \vec{\sigma}_{\xi} = \vec{p}_{\xi} = -2(\vec{e}_x + \sqrt{3}\vec{e}_y)$$

$$\sigma_{\xi\eta} = \vec{\sigma}_{\xi} \vec{e}_{\eta} \rightarrow \sigma_{\xi\eta} = 0 \rightarrow \Delta\beta = D_{\xi\eta} = 0$$

$$\vec{\sigma}_{\eta} = \vec{p}_{\eta} = 3q(-\sqrt{3}\vec{e}_x + \vec{e}_y) \quad (*)$$

$$e) \quad \sigma_{\xi\xi} = \sigma_{11} = \vec{\sigma}_{\xi} \vec{e}_{\xi} \rightarrow \sigma_{11} = \sigma_{\xi\xi} = -2q$$

$$\sigma_{\eta\eta} = \sigma_{22} = \vec{\sigma}_{\eta} \vec{e}_{\eta} \rightarrow \sigma_{22} - \sigma_{\eta\eta} = 6q$$

$$\vec{e}_1 = \vec{e}_{\xi} \quad \vec{e}_2 = \vec{e}_{\eta}$$

Kontrola:

$$\sigma_{11,22} = 2q \pm \sqrt{(2q)^2 + 12q^2} = \begin{cases} 6q \\ -2q \end{cases} \quad \checkmark$$

$$(*) \quad \Delta\gamma = 2\varepsilon_{\mu\nu} = 2 \frac{1+\nu}{E} \sigma_{\mu\nu} = -2 \frac{4\sqrt{3}(1+\nu)}{E}$$

$$\Delta\gamma = D_{\mu\nu} = 4,5 \cdot 10^{-5} q \quad [q \text{ u MPa}]!$$

$$f) \text{ Mises: } (\sigma_{11} - \sigma_{22})^2 + (\sigma_{22} - \sigma_{33})^2 + (\sigma_{33} - \sigma_{11})^2 = 2\sigma_Y^2$$

$$\sigma_{11} = -2q, \quad \sigma_{22} = 6q, \quad \sigma_{33} = 0;$$

$$(-2q - 6q)^2 + (6q)^2 + (2q)^2 = 2\sigma_Y^2$$

$$q_Y = \pm \frac{\sigma_Y}{\sqrt{52}}$$

\rightarrow

$$q_Y = \pm 49,9 \text{ MPa}$$

Ad 2.)

MTT 16.6.97

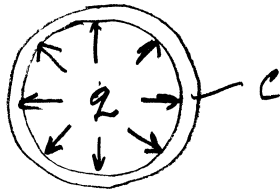
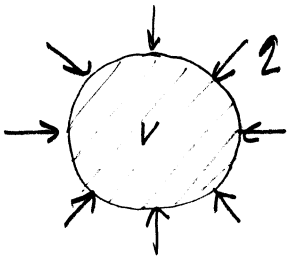
-3-

$$a) \epsilon_{xx}^v = \epsilon_{yy}^v = \epsilon_{ss}^c = \frac{\Delta v - D_0}{D_0} = \frac{200}{199,8} - 1 = 0,001$$

$$\epsilon_{ss}^c = \alpha_T \Delta T = \frac{\Delta v - D_0}{D_0} \rightarrow \Delta T = \frac{\Delta v - D_0}{\alpha_T D_0} =$$
$$= \frac{200 - 199,8}{199,8 \cdot 1,25 \cdot 10^{-5}}$$

$$\Delta T = 80^\circ \text{C}$$

b)



Valf:

$$\sigma_{xx} = \sigma_{yy} = -2$$

$$\sigma_{zz} = 0$$

$$\epsilon_{xx}^v = \frac{1}{E} (\sigma_{xx} - \nu \sigma_{yy}) = -2 \frac{1-\nu}{E}$$

$$\text{cer: } \sigma_{rr} = -2, \sigma_{\theta\theta} = \frac{2Dv}{2\delta}, \sigma_{zz} = 0$$

$$\epsilon_{ss}^c = \frac{1}{E} (\sigma_{\theta\theta} - \nu \sigma_{rr}) - \alpha_T \Delta T = \frac{1}{E} \left(\frac{2Dv}{2\delta} + \nu 2 \right) - \alpha_T \Delta T$$

$$\epsilon_{xx}^v = \epsilon_{ss}^c \rightarrow -2 \frac{1-\nu}{E} = \frac{2}{E} \left(\frac{Dv}{2\delta} + \nu \right) - \alpha_T \Delta T$$

$$2 = \frac{2\delta E \alpha_T \Delta T}{Dv + 2\delta}$$

→

$$2 = 4,305 \text{ MPa}$$

Valf: $\sigma_{xx} = \sigma_{yy} = -4,305 \text{ MPa}$

cer: $\sigma_{rr} = -4,305 \text{ MPa}$

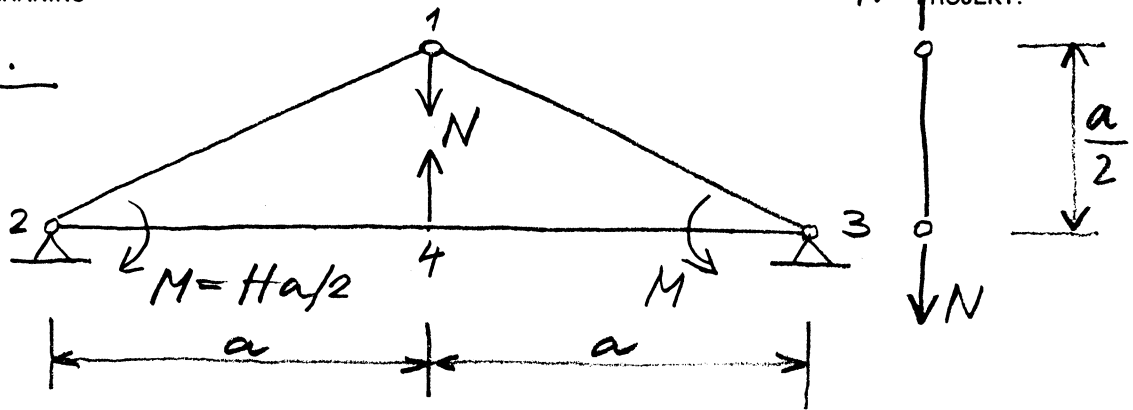
$$\sigma_{ss} = 2 \frac{Dv}{2\delta} \rightarrow$$

$$\sigma_{\theta\theta} = 195,7 \text{ MPa}$$

$$c) \epsilon_{xx}^v = -2 \frac{1-\nu}{E} = \frac{D' - Dv}{Dv} = -4,305 \cdot \frac{1-0,3}{2 \cdot 10^5} = -1,507 \cdot 10^{-5}$$

$$D' = Dv (1 + \epsilon_{xx}^v) \rightarrow D' = 199,997 \text{ mm}$$

Ad 3.



$$w_4 = w_1 + \Delta l_p = w_1 + N \frac{a}{2EA_p}$$

$$w_1 = N \frac{5a\sqrt{5}}{4EA_p} \rightarrow \boxed{w_1 = 0,00998 N}$$

$$w_4 = H \frac{a}{2} \frac{(2a)^2}{8EI_y} - N \frac{(2a)^3}{48EI_y} = H \frac{a^3}{4EI_y} - N \frac{a^3}{6EI_y}$$

$$\boxed{w_4 = 0,44444 - 0,98765 N}$$

$$\Delta l_p = N \frac{a}{2EA_p} \rightarrow \boxed{\Delta l_p = 0,00179 N}$$

$$0,44444 - 0,98765 N = 0,00998 N + 0,00179 N$$

$$\boxed{N = 0,4447 MN}$$

$$w_y(2) = -H \frac{a}{2} \frac{2a}{2EI_y} + N \frac{(2a)^2}{16EI_y} \rightarrow \boxed{w_y(2) = -0,0575}$$

$$u_0 = -\frac{a}{2} w_y(2) + H \frac{\left(\frac{a}{2}\right)^3}{3EI_y} \rightarrow \boxed{u_0 = 0,189 m}$$