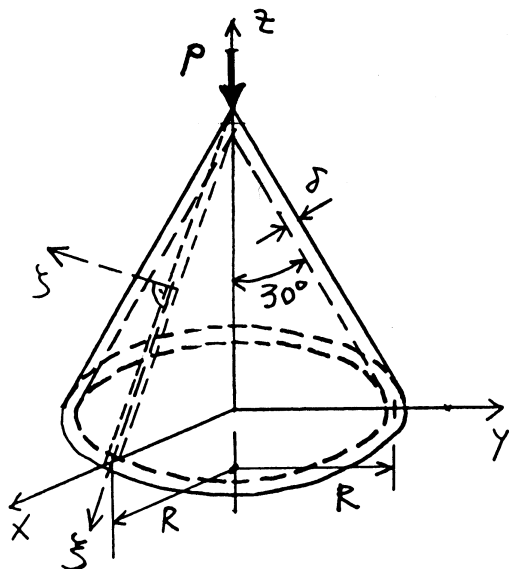


1.



Tanka stožčasta lupina je prilepljena na vodoravno podlago. Srednji polmer osnovne ploskve je R . Vrh stožca je obtežen z navpično silo P . Upoštevajoč, da gre za osnosimetrično napetostno stanje, določi normalno napetost $\sigma_{\xi\xi}$ v steni lupine v odvisnosti od koordinate z ter normalno napetost σ_{zz} in strižno napetost $\sigma_{zx} = \sigma_{zy}$ v osnovni ploskvi ($z = 0$)! Ker gre za tanko lupino ($\delta \ll R$), lahko predpostaviš enakomeren potek napetosti po debelini. Lastne teže lupine ni treba upoštevati.

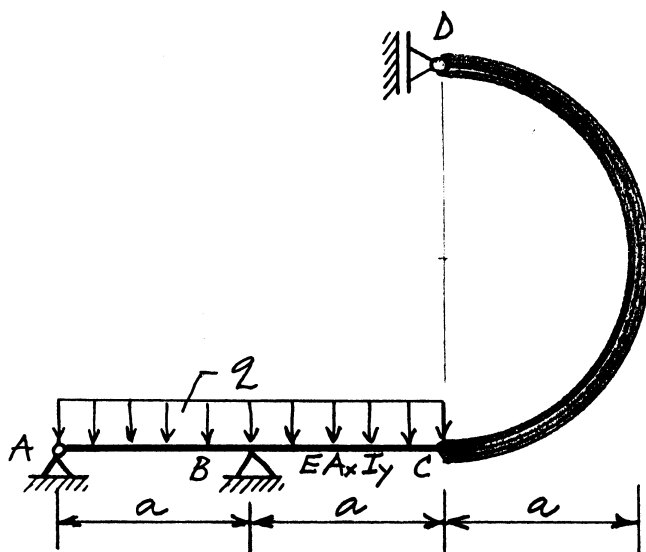
2. Kot rešitev mehanskega problema trdnega telesa smo dobili matriko majhnih deformacij ε_{ij} . V točki $T_0(0, 0, 0)$ je telo nepomično vrtljivo podprto, v točki $T_1(0, 3, 1)$ pa je preprečen navpični pomik u_z .

- Določi vektorsko polje pomikov \vec{u} , ki ustreza podanim deformacijam!
- Določi specifično spremembo razdalje med točkama T_0 in $T_2(0, 0.1, 0.1)$! Kolikšno napako narediš, če to spremembo določiš kar z ustrežno vrednostjo tenzorja majhnih deformacij?
- Določi deformirano telesno koordinatno bazo v točki T_0 !

$$[\varepsilon_{ij}] = 10^{-3} \begin{bmatrix} 0 & 0 & 0 \\ 0 & 10y & z^2 \\ 0 & z^2 & 4yz \end{bmatrix}$$

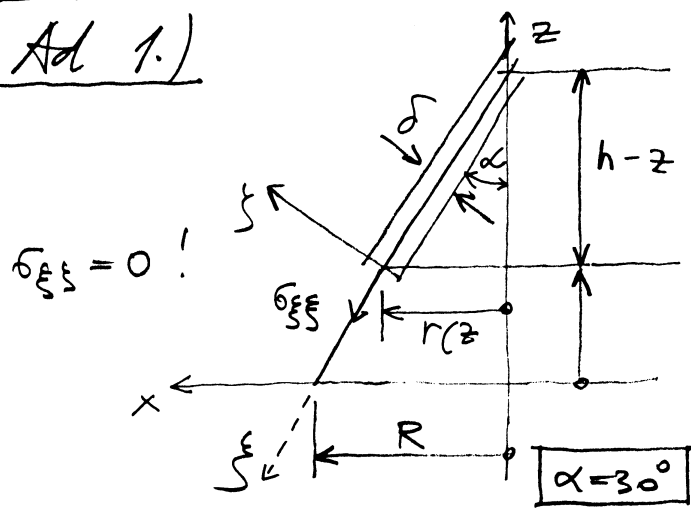
3. Fasadni element \overline{CD} je zelo tog v primerjavi z nosilcem \overline{AC} . V točki C sta oba dela konstrukcije togo povezana.

Določi navpični pomik točke D v odvisnosti od velikosti zvezne obtežbe q !



$$\begin{aligned} E &= 200\,000 \text{ MPa} \\ A_x &= 40 \text{ cm}^2 \\ I_y &= 4000 \text{ cm}^4 \\ a &= 4 \text{ m} \end{aligned}$$

Ad 1.)



$$r(z) = (h-z) \cdot \frac{1}{\sqrt{3}}$$

$$e_{\xi x} = \frac{1}{2}$$

$$e_{\xi z} = -\frac{\sqrt{3}}{2}$$

$$e_{\xi x} = \frac{\sqrt{3}}{2}$$

$$e_{\xi z} = \frac{1}{2}$$

$\sigma_{\xi\xi} = 0!$

$$\Sigma P_z = 0 \rightarrow -P - 2\pi r(z) \cdot \delta \cdot \sigma_{\xi\xi} \cdot \cos \alpha = 0$$

$$\sigma_{\xi\xi} = -\frac{P}{\pi \delta (h-z)} = \sigma_{\xi\xi}(z)$$

$$\sigma_{zz} = \sigma_{\xi\xi} e_{\xi z}^2 = \sigma_{\xi\xi} \cdot \frac{3}{4} \rightarrow \sigma_{zz} = -\frac{3P}{4\pi \delta (h-z)}$$

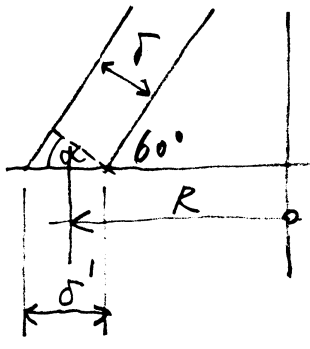
$$\sigma_{zx} = \sigma_{\xi\xi} e_{\xi z} e_{\xi x} = -\sigma_{\xi\xi} \cdot \frac{\sqrt{3}}{4} \rightarrow \sigma_{zx} = \frac{P\sqrt{3}}{4\pi \delta (h-z)}$$

$$z=0 \rightarrow \sigma_{zz} = -\frac{3P}{4\pi \delta h} \quad \sigma_{zx} = \frac{P\sqrt{3}}{4\pi \delta h}$$

Kontrola :

$$\delta' = \frac{\delta}{\cos \alpha} = \frac{2\delta}{\sqrt{3}}, \quad R = \frac{h}{\sqrt{3}}$$

$$-2\pi R \delta' \sigma_{zz}(z=0) - P = 0$$



$$\sigma_{zz}(z=0) = -\frac{3P}{4\pi \delta h} \quad \checkmark$$

Ad 2.) (geij dnyat 26.1.1990)

$$a) \omega_x = \omega_x^0 + \int_0^y \vec{e}_x (\vec{\nabla} \times \vec{E}_y)_{z=0} dy + \int_0^z \vec{e}_x (\vec{\nabla} \times \vec{E}_z) dz$$

$$\vec{e}_x (\vec{\nabla} \times \vec{E}_y) = \begin{vmatrix} 1 & 0 & 0 \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & E_{yy} & E_{yz} \end{vmatrix} = \frac{\partial E_{yz}}{\partial y} - \frac{\partial E_{yy}}{\partial z} = 0$$

$$\vec{e}_x (\vec{\nabla} \times \vec{E}_z) = \begin{vmatrix} 1 & 0 & 0 \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & E_{zy} & E_{zz} \end{vmatrix} = \frac{\partial E_{zz}}{\partial y} - \frac{\partial E_{yz}}{\partial z} = 2z \cdot 10^{-3}$$

$$\omega_x = \omega_x^0 + 10^{-3} \int_0^z 2z dz \rightarrow \boxed{\omega_x = \omega_x^0 + 10^{-3} z^2 = \omega_{yz}}$$

$$u_y = u_y^0 + \int_0^y (E_{yy})_{z=0} dy + \int_0^z (E_{zy} + \omega_{yz}) dz$$

$$u_y = 0 + 10^{-3} \left(\int_0^y 10y dy + \int_0^z (z^2 - \omega_x^0 \cdot 10^3 - z^2) dz \right)$$

$$\boxed{u_y = -z \omega_x^0 + 5y^2 \cdot 10^{-3}}$$

$$u_z = u_z^0 + \int_0^y (E_{yz} + \omega_{yz})_{z=0} dy + \int_0^z E_{zz} dz$$

$$u_z = 10^{-3} \left(\int_0^y (z^2 + 10^3 \omega_x^0 + z^2)_{z=0} dy + \int_0^z 4yz dz \right)$$

$$\boxed{u_z = y \omega_x^0 + 2yz^2 \cdot 10^{-3}}$$

$$u_z(T_1) = 3 \omega_x^0 + 2 \cdot 3 \cdot 1 \cdot 10^{-3} = 0$$

$$\boxed{\omega_x^0 = -2 \cdot 10^{-3}}$$

$$\boxed{\vec{u} = [(5y^2 + 2z) \vec{e}_y + 2y(z^2 - 1) \vec{e}_z] \cdot 10^{-3}}$$

$$b) \quad \Delta \vec{r} = \vec{r}_2 - \vec{r}_0 = 0,1 \vec{e}_y + 0,1 \vec{e}_z \rightarrow |\Delta \vec{r}| = 0,14142$$

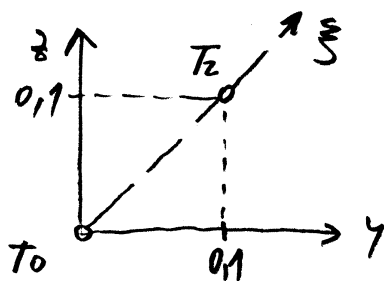
$$\vec{u}_2 = 10^{-3} [(5 \cdot 0,1^2 + 2 \cdot 0,1) \vec{e}_y + 2 \cdot 0,1 (0,1^2 - 1) \vec{e}_z]$$

$$\vec{u}_2 = 10^{-3} [0,250 \vec{e}_y - 0,198 \vec{e}_z]$$

$$\vec{r}_2' = \vec{r}_2 + \vec{u}_2 = 0,10025 \vec{e}_y + 0,09980 \vec{e}_z = \Delta \vec{r}'$$

$$|\Delta \vec{r}'| = 0,14146$$

$$\Delta(T_0, T_2) = \frac{|\Delta \vec{r}'|}{|\Delta \vec{r}|} - 1 \rightarrow \boxed{D = 0,2657 \cdot 10^{-3}}$$



$$e_{\xi y} = e_{\xi z} = \frac{\sqrt{2}}{2}$$

$$\epsilon_{\xi\xi\xi} \approx D = \epsilon_{yy} e_{\xi y} + 2\epsilon_{yz} e_{\xi y} e_{\xi z} + \epsilon_{zz} e_{\xi z} = 0$$

$\epsilon_{ij}(T_0) = 0$... Naprava je mehonično relaksa.

$$c) \quad \frac{\partial \vec{u}}{\partial y} = 10^{-3} [104 \vec{e}_y + 2(z^2 - 1) \vec{e}_z]$$

$$\frac{\partial \vec{u}}{\partial z} = 10^{-3} [2 \vec{e}_y + 4yz \vec{e}_z]$$

$$\vec{e}_y' = \vec{e}_y + \frac{\partial \vec{u}}{\partial y}$$

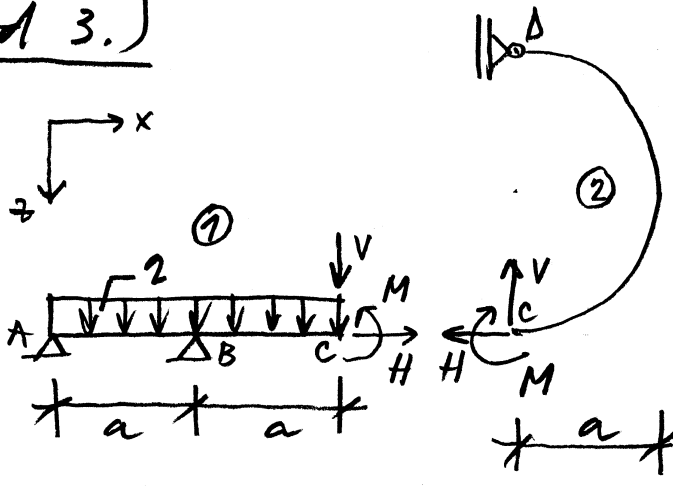
$$\vec{e}_y' = (1 + 0,01y) \vec{e}_y + 0,002(z^2 - 1) \vec{e}_z$$

$$\vec{e}_z' = \vec{e}_z + \frac{\partial \vec{u}}{\partial z}$$

$$\vec{e}_z' = 0,002 \vec{e}_y + (1 + 0,004yz) \vec{e}_z$$

$$T_0: \left\{ \begin{array}{l} \vec{e}_y' = \vec{e}_y - 0,002 \vec{e}_z \\ \vec{e}_z' = 0,002 \vec{e}_y + \vec{e}_z \end{array} \right.$$

Ad 3.)



② : $V=0$
 $H \cdot 2a + M = 0$

$$H = -M \frac{1}{2a}$$

$$\begin{aligned} \vec{r}_D &= -2a \vec{e}_z \\ \vec{u}_C &= u_C \vec{e}_x + w_C \vec{e}_z \\ \vec{\omega}_C &= \omega_C \vec{e}_y \end{aligned}$$

$$\vec{u}_D = \vec{u}_C + \vec{\omega}_C \times \vec{r}_D = u_C \vec{e}_x + w_C \vec{e}_z - 2a \omega_C \vec{e}_x$$

$$\vec{u}_D = (u_C - 2a \omega_C) \vec{e}_x + w_C \vec{e}_z \rightarrow \boxed{w_D = w_C}$$

$$u_x(D) = u_D = 0 \rightarrow$$

$$\boxed{u_C = 2a \omega_C}$$

① $w_C = \frac{2a^4}{4EI_y} - M \frac{5a^2}{6EI_y}$

$$\omega_C = -2 \frac{7a^3}{24EI_y} + M \frac{4a}{3EI_y}$$

$$u_C = H \frac{a}{EA_x} = 2a \left(-2 \frac{7a^3}{24EI_y} + M \frac{4a}{3EI_y} \right)$$

$$-\frac{M}{2a} \cdot \frac{a}{A_x} = -2 \frac{7a^4}{12EI_y} + M \frac{8a^2}{3EI_y}$$

$$\boxed{M = 2 \frac{7a^4 A_x}{2(3I_y + 16a^2 A_x)}}$$

$$\rightarrow \boxed{M = 34996 \text{ N}}$$

$$\boxed{w_C = w_D = 2,167 \text{ m}}$$